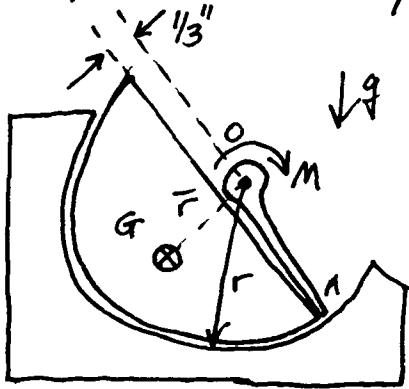


### Example: Ice tray

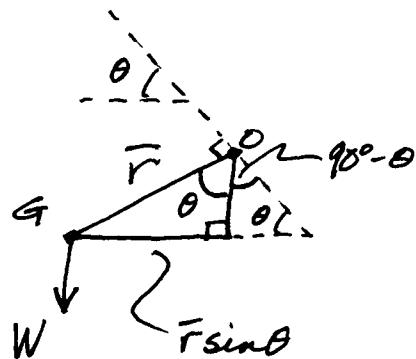
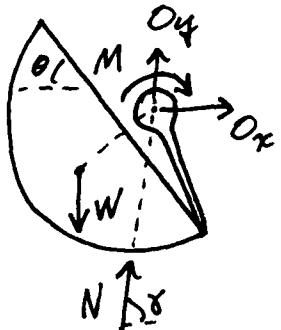


$$r = 1.5"$$

$$\bar{r} = 0.55r$$

Arm OA ejects the ice cubes from the tray. There are 8 "cubes" with a total combined weight of 0.56 lb. Neglecting friction, and assuming that the resultant of the normal force of the tray on the cubes acts through O, determine the total moment  $M$  on all 8 cubes as a function of  $\theta$ . (neglect weight of arm)

FBD ("cube" - arm system)



This FBD has 5 unknowns,  $O_x$ ,  $O_y$ ,  $M$ ,  $N$  and  $\lambda$ . In general we would not be able to solve for any of these quantities from an equilibrium analysis of this FBD alone. However, since  $O_x$ ,  $O_y$  and  $N$  act through O, taking moments about O will yield a relationship between  $M$  and  $W$ .

$$\sum M_O^{\circ} = W\bar{r}\sin\theta - M = 0 \rightarrow M = W\bar{r}\sin\theta$$

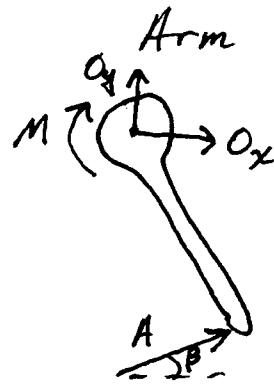
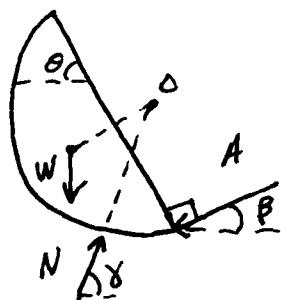
$$M = 0.56(1.5 \cdot 0.55)\sin\theta = 0.462\sin\theta$$

If we do want  $N, \gamma, O_x$  and  $O_y$ ,  $\sum F_x = 0$  and  $\sum F_y = 0$  do not provide enough equations to solve for all of these quantities.

However, we can break the system into components to determine if we can find additional equations without introducing too many more unknowns.

### Component FBDs

"Cube"



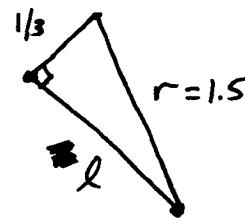
$$\beta = 90^\circ - \theta$$

Now we could get  $A, N$  and  $\gamma$  from the equilibrium analysis of the "cube" and we could then ~~determine~~ determine  $O_x, O_y$  and  $M$  from the equilibrium analysis of the arm.

~~This problem has been solved for you.~~

"Cube" equilibrium:

$$\sum M_z^o = W \bar{r} \sin \theta - Al = 0$$



$$\begin{aligned} l &= \sqrt{1.5^2 - (\frac{1}{3})^2} \\ &= 1.462'' \end{aligned}$$

$$\rightarrow A = \frac{W \bar{r} \sin \theta}{l} = 0.316 \sin \theta$$

$$\sum F_x = N \cos \gamma - A \underbrace{\cos \beta}_{=\sin \theta} = 0$$

$$\rightarrow N \cos \gamma = A \sin \theta = 0.316 \sin^2 \theta$$

$$\sum F_y = N \sin \gamma - A \underbrace{\sin \beta}_{=\cos \theta} - W = 0$$

$$\rightarrow N \sin \gamma = W + A \cos \theta = 0.56 + 0.316 \sin \theta \cos \theta$$

$$\rightarrow N = \sqrt{(W + A \cos \theta)^2 + (A \sin \theta)^2}$$

$$\gamma = \arctan \left( \frac{W + A \cos \theta}{A \sin \theta} \right)$$

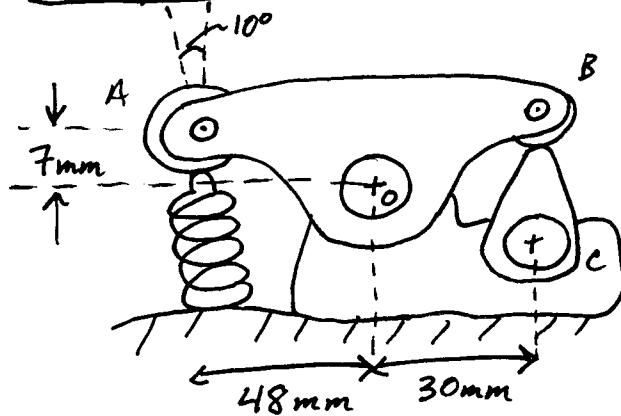
Arm Equilibrium:  $\sum M_z^o = Al - M = 0$

$$\rightarrow M = W \bar{r} \sin \theta = 0.462 \sin \theta \quad (\checkmark \text{ same as before})$$

$$\sum F_x = O_x + A \underbrace{\cos \beta}_{\sin \theta} = 0 \rightarrow O_x = -A \sin \theta$$

$$\sum F_y = O_y + A \underbrace{\sin \beta}_{\cos \theta} = 0 \rightarrow O_y = -A \cos \theta$$

### Example : Cam - Rocker - Valve

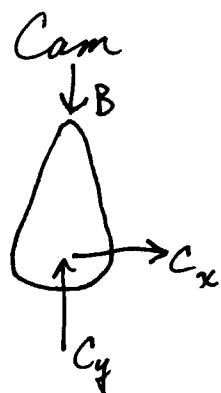
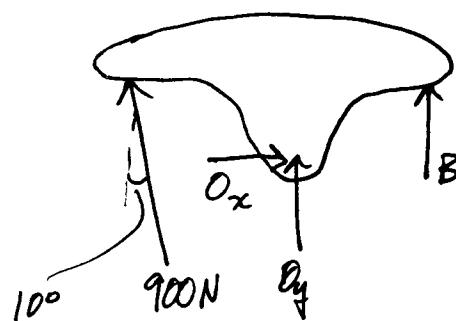
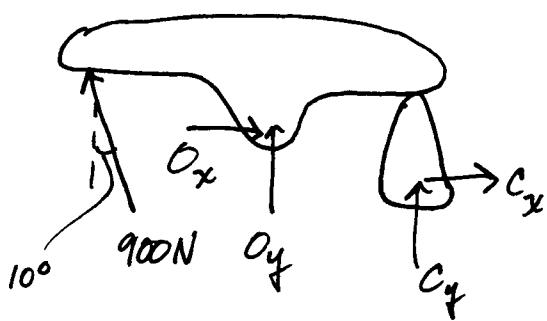


Spring force is 900 N.  
Determine the reaction forces at O and C.

### FBDs

Rocker + Cam

Rocker



Equilibrium analysis : Rocker only

$$\sum M_O^o = B(30) - 900 \cos 10^\circ (48) + 900 \sin 10^\circ (7) = 0$$

$$\rightarrow B = 1382 \text{ N}$$

$$\begin{aligned}\sum F_x &= -900 \sin 10^\circ + O_x = 0 \\ \rightarrow O_x &= 156 N\end{aligned}$$

$$\begin{aligned}\sum F_y &= 900 \cos 10^\circ + B + O_y = 0 \\ \rightarrow O_y &= -2268 N\end{aligned} \quad \left. \begin{array}{l} O = \sqrt{156^2 + 2268^2} \\ = 2273 N \end{array} \right\}$$

Cam:  $\sum F_x = 0 \rightarrow C_x = 0$

$$\sum F_y = C_y - B = 0 \rightarrow C_y = B = 1382 N$$

Cam-Rocker System:  $\sum F_x = -900 \sin 10^\circ + O_x + C_x = 0$   
Same as  $\sum F_x^{\text{cam}} + \sum F_x^{\text{rocker}} = 0$

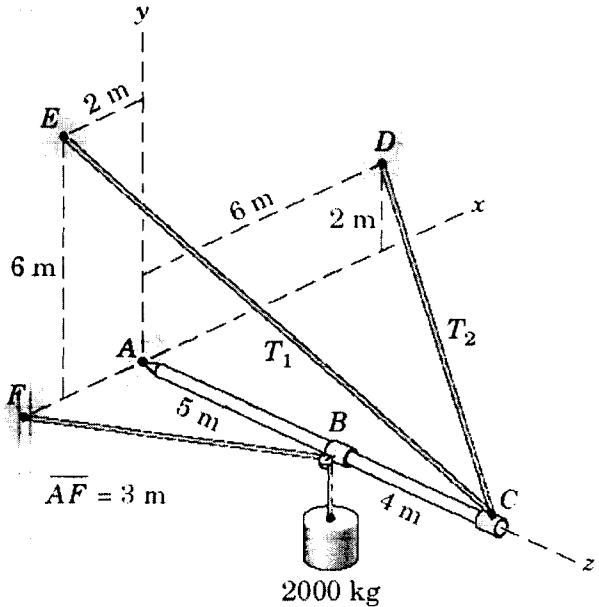
$$\sum F_y = 900 \cos 10^\circ + O_y + C_y = 0$$

Same as  $\sum F_y^{\text{cam}} + \sum F_y^{\text{rocker}} = 0$

$$\begin{aligned}\sum M_z^o &= -900 \cos 10^\circ (48) + 900 \sin 10^\circ (7) \\ &\quad + C_y (30) + C_x d_L = 0\end{aligned}$$

Same as  $\sum M_z^o, \text{cam} + \sum M_z^o, \text{rocker} = 0$

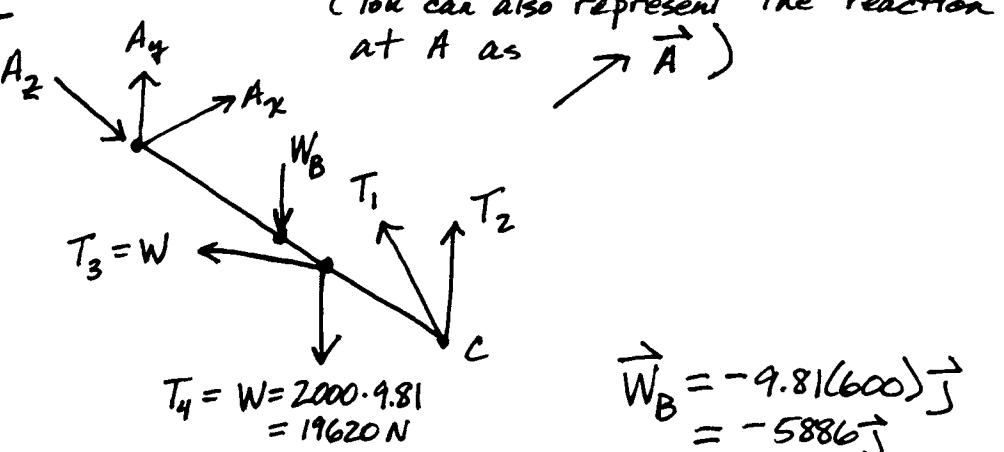
Considering the equilibrium equations for the ~~the~~ entire system always give 3 redundant equations (i.e. not new) if the equilibrium equations for each individual component have already been determined.



The 9-m steel beam has a mass of 600 kg with center of mass at midlength. It is supported by a ball and socket joint at A and the two cables under tensions  $T_1$  and  $T_2$ .

- calculate the tensions  $T_1$  and  $T_2$  and the reactions at A.
- Determine a "quick" method of solution if only the tension  $T_1$  is asked for.

a) FBD



Vector representations:  $\vec{A} = A_x \vec{i} + A_y \vec{j} + A_z \vec{k}$   
(All numerical values of forces are in Newtons)

$$\vec{T}_4 = -19620 \vec{j}$$

$$\vec{T}_3 = 19620 \frac{-3\vec{i} - 5\vec{k}}{\sqrt{3^2 + 5^2}} = -10094 \vec{i} - 16824 \vec{k}$$

(62)

$$\vec{T}_1 = T_1 \frac{-2\vec{z} + 6\vec{j} - 9\vec{k}}{\sqrt{z^2 + 6^2 + 9^2}} = T_1 \left( -\frac{2}{11}\vec{z} + \frac{6}{11}\vec{j} - \frac{9}{11}\vec{k} \right)$$

$$\vec{T}_2 = T_2 \frac{6\vec{z} + 2\vec{j} - 9\vec{k}}{\sqrt{z^2 + 6^2 + 9^2}} = T_2 \left( \frac{6}{11}\vec{z} + \frac{2}{11}\vec{j} - \frac{9}{11}\vec{k} \right)$$

We will be taking moments about A, so we need the moments of each of these forces about A.

$$\begin{aligned}\vec{M}_1^A &= \vec{r}_{AC} \times \vec{T}_1 = 9\vec{k} \times T_1 \left( -\frac{2}{11}\vec{z} + \frac{6}{11}\vec{j} - \frac{9}{11}\vec{k} \right) \\ &= -\frac{18}{11}T_1 \vec{k} \times \vec{z} + \frac{54}{11}T_1 \vec{k} \times \vec{j} \\ &= -\frac{54}{11}T_1 \vec{z} - \frac{18}{11}T_1 \vec{j}\end{aligned}$$

$$\begin{aligned}\vec{M}_2^A &= \vec{r}_{AC} \times \vec{T}_2 = 9\vec{k} \times T_2 \left( \frac{6}{11}\vec{z} + \frac{2}{11}\vec{j} - \frac{9}{11}\vec{k} \right) \\ &= \frac{54}{11}T_2 \vec{k} \times \vec{z} + \frac{18}{11}T_2 \vec{k} \times \vec{j} \\ &= -\frac{18}{11}T_2 \vec{z} + \frac{54}{11}T_2 \vec{j}\end{aligned}$$

$$\begin{aligned}\vec{M}_{34}^A &= \vec{r}_{AB} \times (\vec{T}_3 + \vec{T}_4) = 5\vec{k} \times (-10094\vec{z} - 19620\vec{j} - 16824\vec{k}) \\ &= -5(10094)\vec{k} \times \vec{z} - 5(19620)\vec{k} \times \vec{j} \\ &= 98100\vec{z} - 50470\vec{j}\end{aligned}$$

$$\vec{M}_{W_B}^A = \vec{r}_{cm} \times \vec{W}_B = 4.5\vec{k} \times (-5886\vec{j}) = 26487\vec{z}$$

### Equilibrium

$$\begin{aligned}\sum M_z^A &= -\frac{54}{11}T_1 \vec{z} - \frac{18}{11}T_1 \vec{j} \\ &\quad - \frac{18}{11}T_2 \vec{z} + \frac{54}{11}T_2 \vec{j} \\ &\quad + 98100\vec{z} - 50470\vec{j} \quad \text{[cancel]} \\ &\quad + 26487\vec{z} \\ &= 0\end{aligned}$$

(63)

$$\vec{z} \text{ components} \rightarrow \frac{54}{11} T_1 + \frac{18}{11} T_2 = 98100 + 26487 \quad (A)$$

$$\vec{j} \text{ components} \rightarrow -\frac{18}{11} T_1 + \frac{54}{11} T_2 = 50470 \quad (B)$$

$$54(A) - 18(B) \rightarrow \left( \frac{54 \cdot 54}{11} + \frac{18 \cdot 18}{11} \right) T_1 = 124587(54) - 50470(18)$$

$$\rightarrow T_1 = 19757 \text{ N}$$

$$\rightarrow T_2 = 16866 \text{ N}$$

Then:  ~~$\sum \vec{F}$~~   $\sum \vec{F} = 19757 \left( -\frac{2}{11} \vec{z} + \frac{6}{11} \vec{j} - \frac{9}{11} \vec{k} \right)$   
 $+ 16866 \left( \frac{6}{11} \vec{z} + \frac{2}{11} \vec{j} - \frac{9}{11} \vec{k} \right)$   
 $- 10094 \vec{z} \qquad \qquad \qquad - 16824 \vec{k}$   
 $- 19620 \vec{j}$   
 $- 5886 \vec{j}$   
 $+ A_x \vec{z} + A_y \vec{j} + A_z \vec{k} = 0$

$$\vec{z} \rightarrow A_x = 10094 - 16866 \left( \frac{6}{11} \right) + 19757 \left( \frac{2}{11} \right) = 4487 \text{ N}$$

$$\vec{j} \rightarrow A_y = 5886 + 19620 - 16866 \left( \frac{2}{11} \right) - 19757 \left( \frac{6}{11} \right) = 11663 \text{ N}$$

$$\vec{k} \rightarrow A_z = 16824 + 16866 \left( \frac{9}{11} \right) + 19757 \left( \frac{9}{11} \right) = 46788 \text{ N}$$

(64)

- b) If we are only interested in  $T_1$ , then we want to find a point or an axis about which the moments due to all of the other unknown forces are zero.

Our unknown forces are those at A,  $T_1$ , and  $T_2$ . The forces at A have zero moment about point A and any axis passing through A, and  $T_2$  has zero moment about any axis passing through D. (Note that all of the forces in this problem have zero moment about the axis AC.) If we take moments about the axis AD, the only unknown force that appears is due to  $T_1$ .

$$\vec{e}_{AD} = \frac{6\vec{i} + 2\vec{j}}{\sqrt{6^2 + 2^2}} = \frac{3}{\sqrt{10}}\vec{i} + \cancel{\frac{1}{\sqrt{10}}}\vec{j}$$

$$M_1^{AD} = \vec{M}_1^A \cdot \vec{e}_{AD} = \left( -\frac{54}{11} \frac{3}{\sqrt{10}} - \frac{18}{11} \frac{1}{\sqrt{10}} \right) T_1 = \frac{-180}{11\sqrt{10}} T_1$$

$$M_{34}^{AD} = \vec{M}_{34}^A \cdot \vec{e}_{AD} = 98100 \frac{3}{\sqrt{10}} - 50470 \frac{1}{\sqrt{10}} = \frac{243830}{\sqrt{10}}$$

$$M_{WB}^{AD} = \vec{M}_{WB}^A \cdot \vec{e}_{AD} = 26487 \frac{3}{\sqrt{10}} = \frac{79461}{\sqrt{10}}$$

$$\sum M^{AD} = \frac{-180}{11\sqrt{10}} T_1 + \frac{243830 + 79461}{\sqrt{10}} = 0$$

↗  $T_1 = 19757 \text{ N}$

You do not need this in vector form because all of these moments are in the same  $\vec{e}_{AD}$  direction.