



THE UNIVERSITY OF TEXAS AT AUSTIN

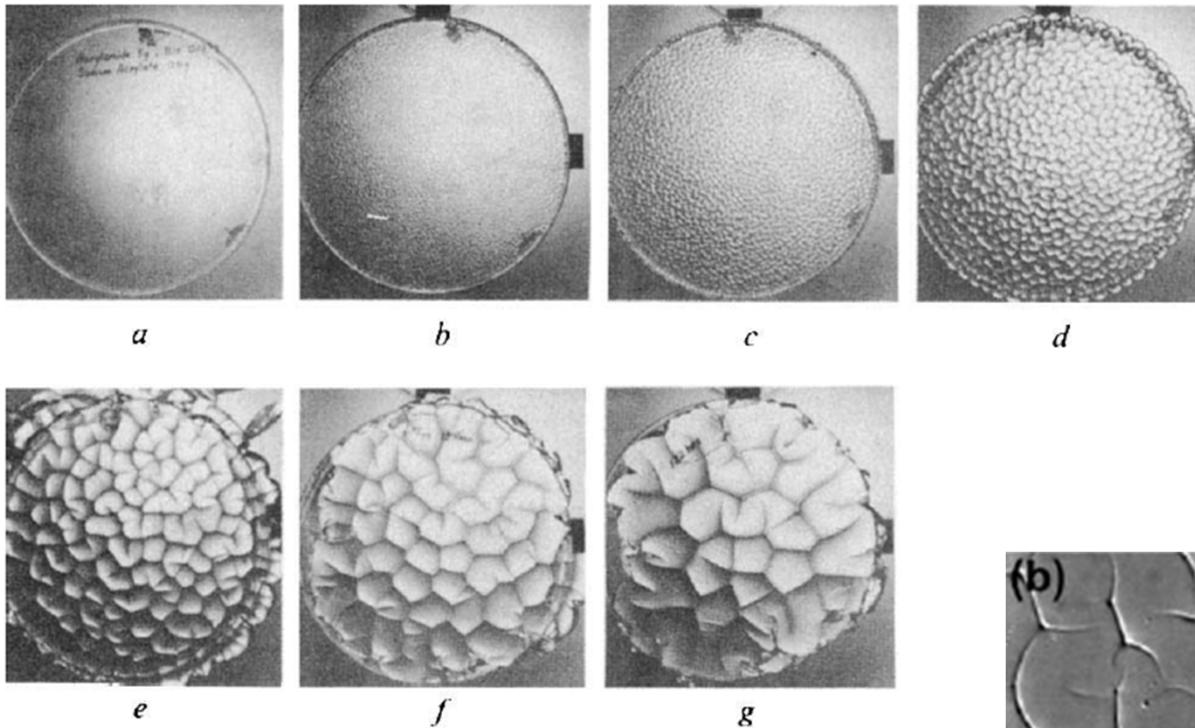
AEROSPACE ENGINEERING  
& ENGINEERING MECHANICS

# **Swell-Induced Surface Instability in Substrate-Confined Hydrogel Layer**

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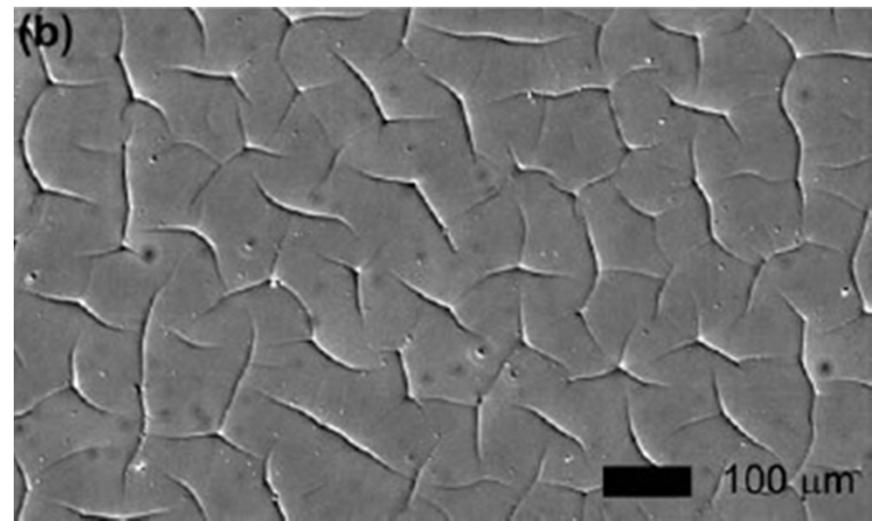
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# Swelling of rubber and gels



- Southern and Thomas, 1965
- Tanaka et al, 1987
- Trujillo et al., 2008

- Critical condition for the onset of surface instability?
- Any characteristic size?
- Effect of kinetics?



# A theoretical framework for gels

Free energy density function

$$U(\mathbf{F}, C)$$

Nominal stress

$$s_{iK} = \frac{\partial U}{\partial F_{iK}}$$

Volume change

$$\det(\mathbf{F}) = 1 + vC$$

Chemical potential

$$\mu = \frac{\partial U}{\partial C}$$

Equilibrium equations

$$\frac{\partial s_{iK}}{\partial X_K} + B_i = 0$$

$$\frac{\partial \mu}{\partial X_K} = 0$$

Boundary conditions

$$T_i = s_{iK} N_K \quad \text{or} \quad \delta x_i = 0 \quad \mu = \mu_{ext}$$

- Hong, Zhao, Zhou, and Suo, JMPS 2008

# A specific material model

Free energy density function

$$U(\mathbf{F}, C) = U_e(\mathbf{F}) + U_m(C)$$

**Neo-Hookean rubber elasticity:**

$$U_e(\mathbf{F}) = \frac{1}{2} N k_B T [F_{iK} F_{iK} - 3 - 2 \ln(\det(\mathbf{F}))]$$

**Flory-Huggins polymer solution theory:**

$$U_m(C) = \frac{k_B T}{\nu} \left[ \nu C \ln\left(\frac{\nu C}{1+\nu C}\right) + \frac{\chi \nu C}{1+\nu C} \right]$$

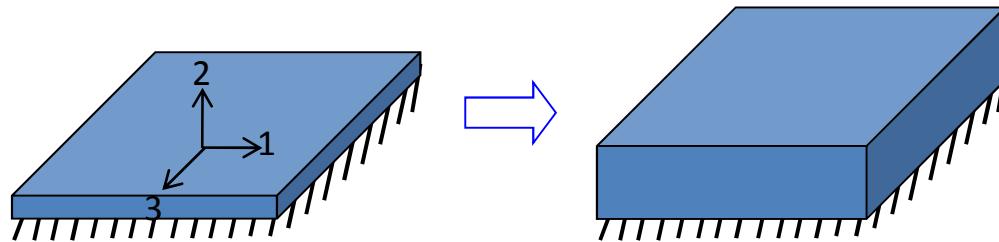
$Nk_B T$  : initial shear modulus of the polymer network

$N$  : No. of polymer chains per unit volume

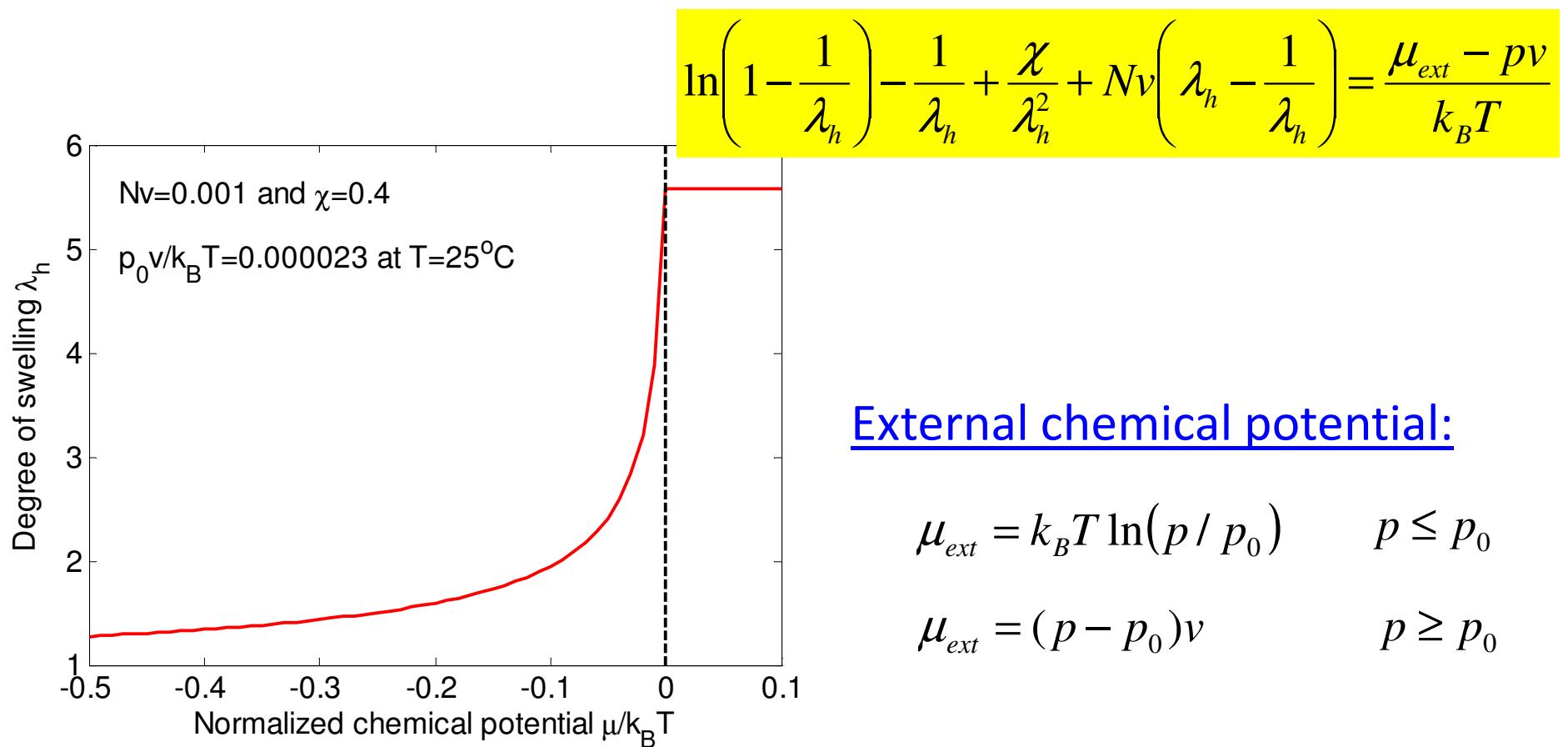
$\nu$  : Volume of a solvent molecule

$\chi$  : Enthalpy of mixing parameter

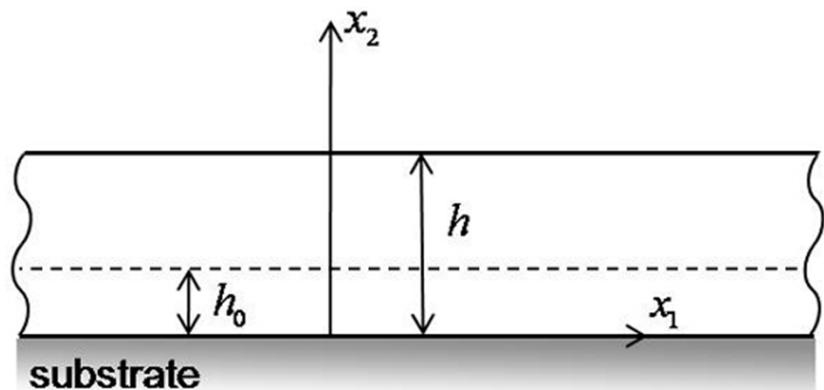
# Homogeneous swelling of a hydrogel layer



$$\begin{aligned}\lambda_1 &= \lambda_3 = 1 \\ \lambda_2 &= \lambda_h > 1\end{aligned}$$

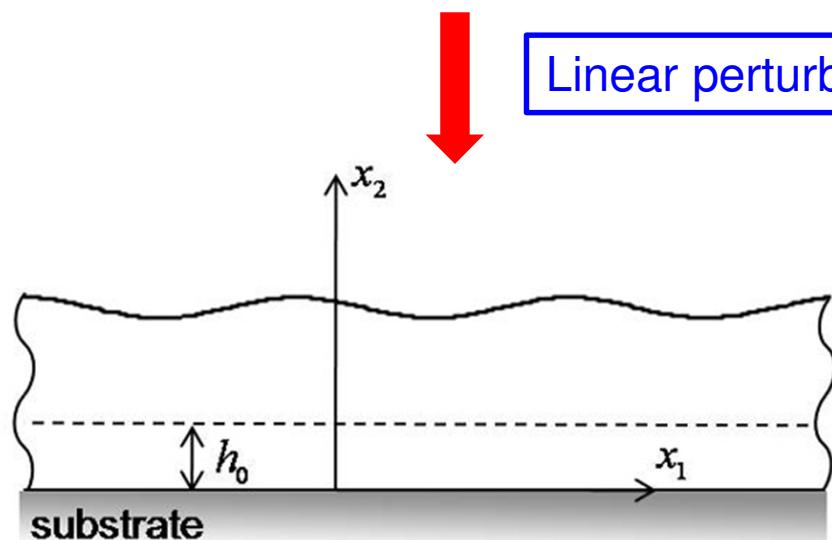


# A linear perturbation analysis



Homogeneous swelling

$$\mathbf{F} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \lambda_h & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



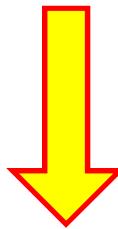
Linear perturbation:

$$u_1 = u_1(x_1, x_2), u_2 = u_2(x_1, x_2)$$

$$\tilde{\mathbf{F}} = \begin{bmatrix} 1 + \frac{\partial u_1}{\partial x_1} & \lambda_h \frac{\partial u_1}{\partial x_2} & 0 \\ \frac{\partial u_2}{\partial x_1} & \lambda_h \left( 1 + \frac{\partial u_2}{\partial x_2} \right) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

# Linearized equilibrium equations

$$(1 + \lambda_h \xi_h) \frac{\partial^2 u_1}{\partial x_1^2} + \lambda_h^2 \frac{\partial^2 u_1}{\partial x_2^2} + \lambda_h \xi_h \frac{\partial^2 u_2}{\partial x_1 \partial x_2} = 0$$
$$\frac{\partial^2 u_2}{\partial x_1^2} + \lambda_h (\xi_h + \lambda_h) \frac{\partial^2 u_2}{\partial x_2^2} + \lambda_h \xi_h \frac{\partial^2 u_1}{\partial x_1 \partial x_2} = 0$$



Solution by the method  
of Fourier transform

$$\begin{cases} \hat{u}_1(x_2; k) = \sum_{n=1}^4 A_n \bar{u}_1^{(n)} \exp(q_n x_2) \\ \hat{u}_2(x_2; k) = \sum_{n=1}^4 A_n \bar{u}_2^{(n)} \exp(q_n x_2) \end{cases}$$

# Critical Conditions for Surface Instability

Boundary conditions

$$\begin{cases} s_{22} = -p \left( 1 + \frac{\partial u_1}{\partial x_1} \right) & \text{at } x_2 = h \\ s_{12} = p \frac{\partial u_2}{\partial x_1} & \text{at } x_2 = h \\ u_1 = u_2 = 0 & \text{at } x_2 = 0 \end{cases}$$



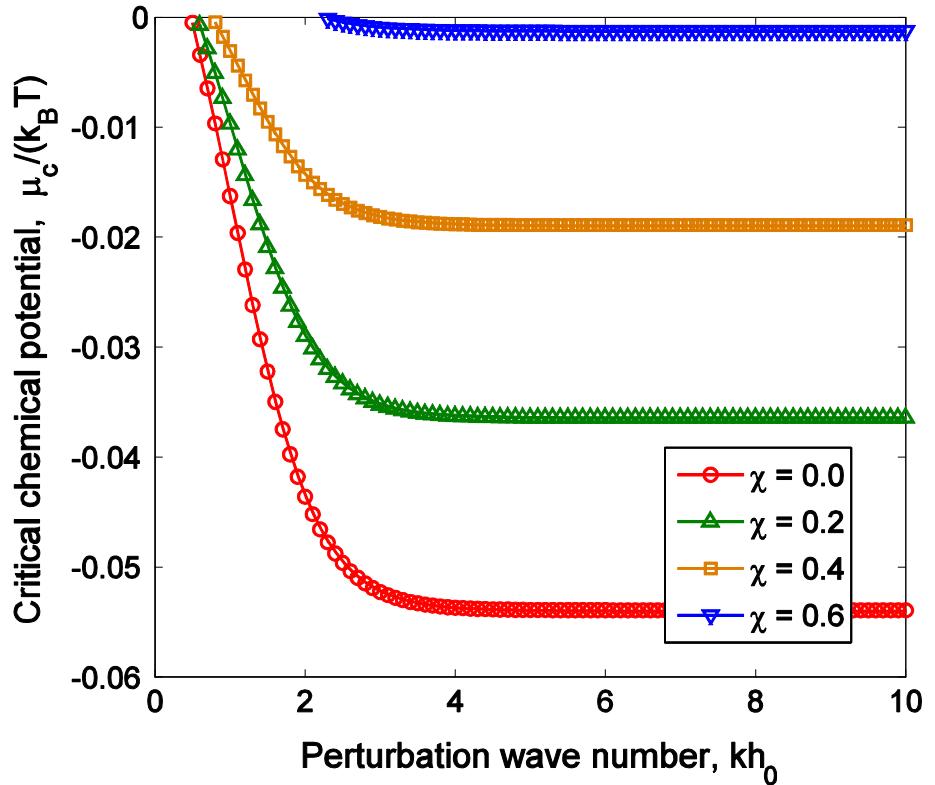
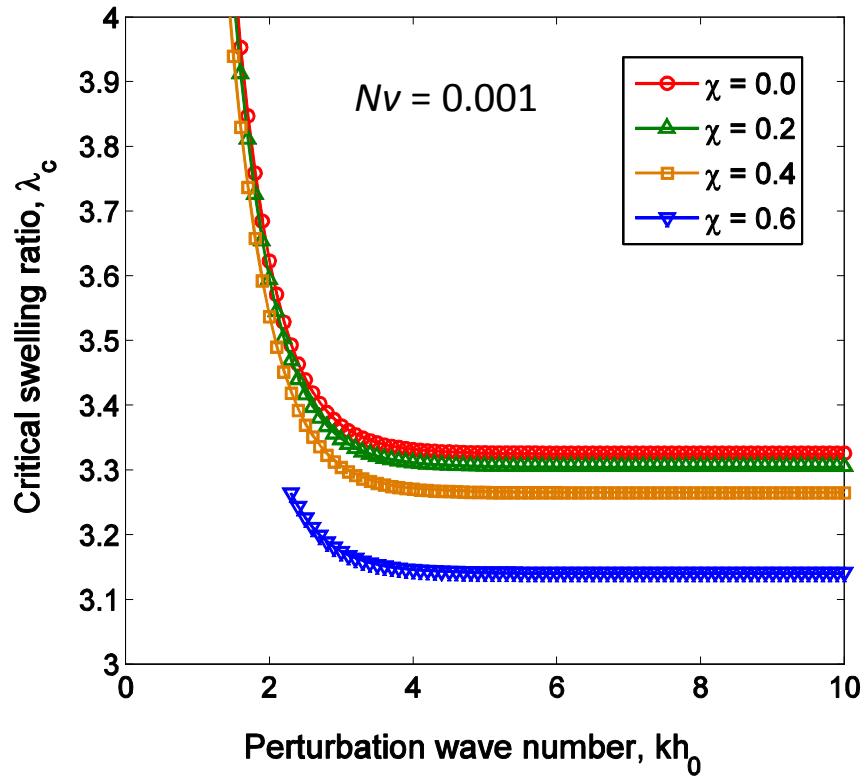
$$\sum_{n=1}^4 D_{mn} A_n = 0$$

$$[D_{mn}] = \begin{bmatrix} 1 & 1 & 1 & 1 \\ -\lambda_h & \lambda_h & -\beta & \beta \\ 2\lambda_h e^{kh_0} & 2\lambda_h e^{-kh_0} & \left(\lambda_h + \frac{1}{\lambda_h}\right) e^{\beta kh} & \left(\lambda_h + \frac{1}{\lambda_h}\right) e^{-\beta kh} \\ \left(\lambda_h + \frac{1}{\lambda_h}\right) e^{kh_0} & -\left(\lambda_h + \frac{1}{\lambda_h}\right) e^{-kh_0} & 2\beta e^{\beta kh} & -2\beta e^{-\beta kh} \end{bmatrix}$$

**Critical condition:**

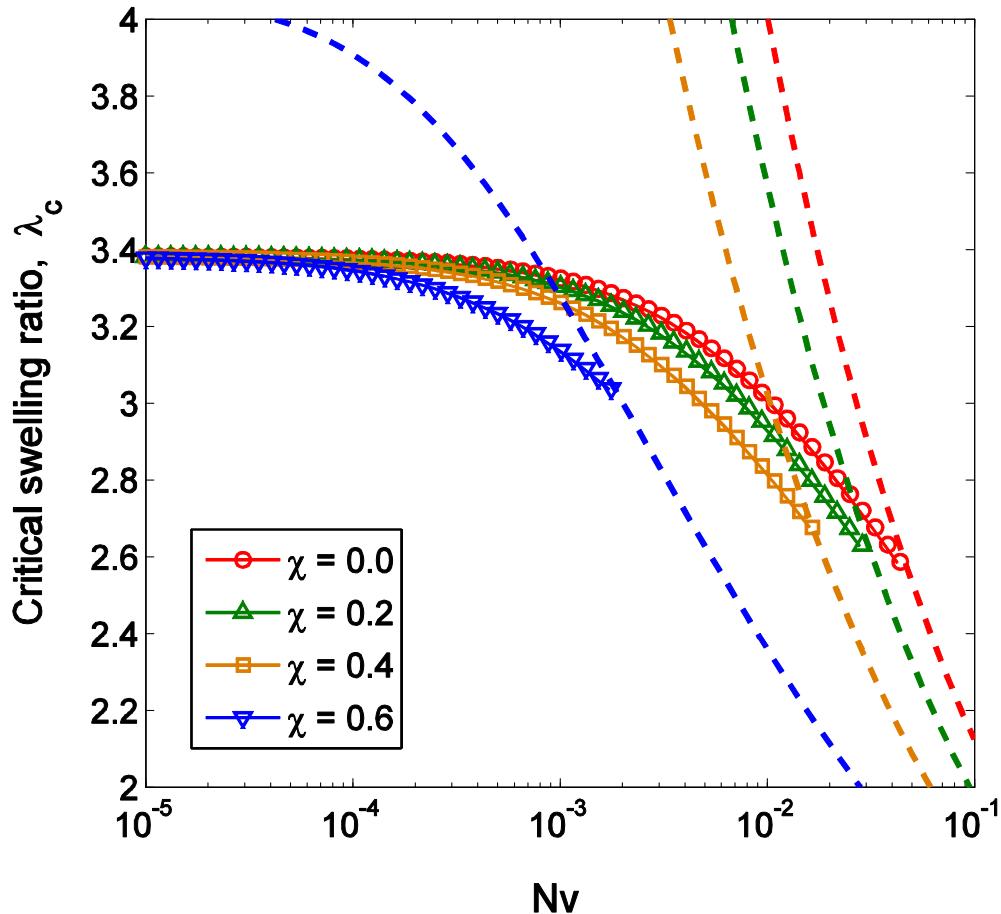
$$\det[D_{mn}] = f(kh_0, \lambda_h; Nv, \chi) = 0$$

# Effect of perturbation wave number



- Long wavelength perturbation is stabilized by the substrate effect.
- Short wavelength perturbation is unaffected.
- Thus the critical condition can be taken at the short-wavelength limit.

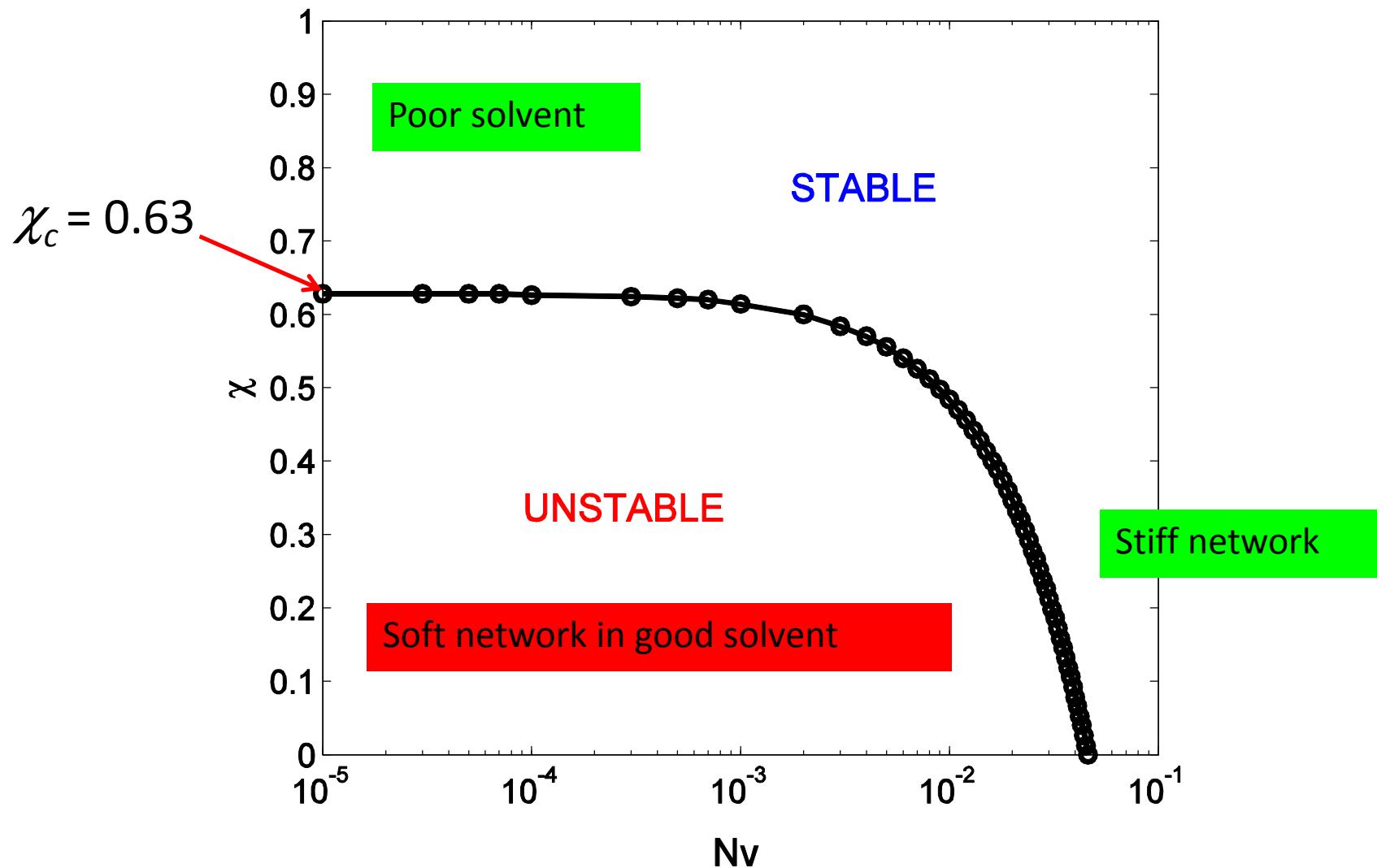
# Short-wave limit ( $kh_0 \rightarrow \infty$ )



$$\left( \lambda_h + \frac{1}{\lambda_h} \right)^2 = 4\lambda_h \beta$$

- The critical swelling ratio depends on  $Nv$  and  $\chi$ , ranging between 2.5 and 3.4.
- For each  $\chi$ , there exists a critical value for  $Nv$ .
- For small  $Nv$  ( $< 10^{-4}$ ), the critical swelling ratio is nearly a constant ( $\sim 3.4$ ).

# A stability diagram



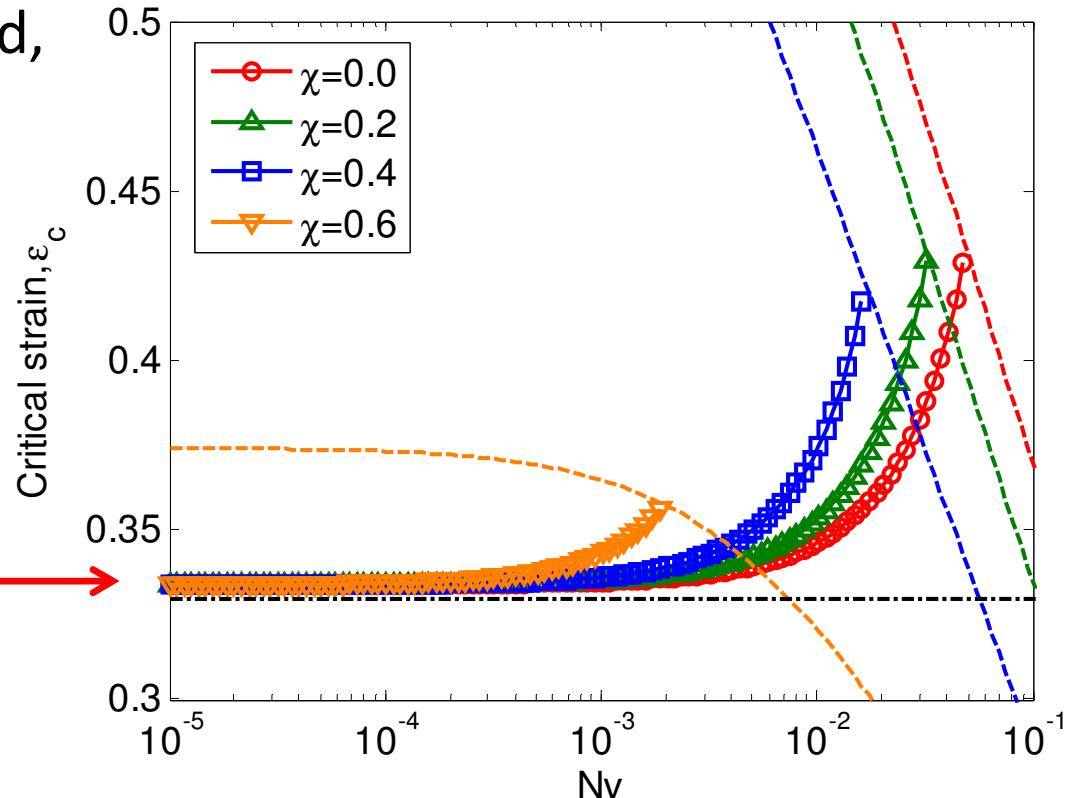
Kang and Huang, J. Mech. Phys. Solids 58, 1582-1598 (2010).

# Critical linear strain

Relative to the unconstrained,  
free swelling in 3D:

$$\varepsilon = \frac{\lambda_{3D} - 1}{\lambda_{3D}}$$

$$\varepsilon_c = 0.33$$

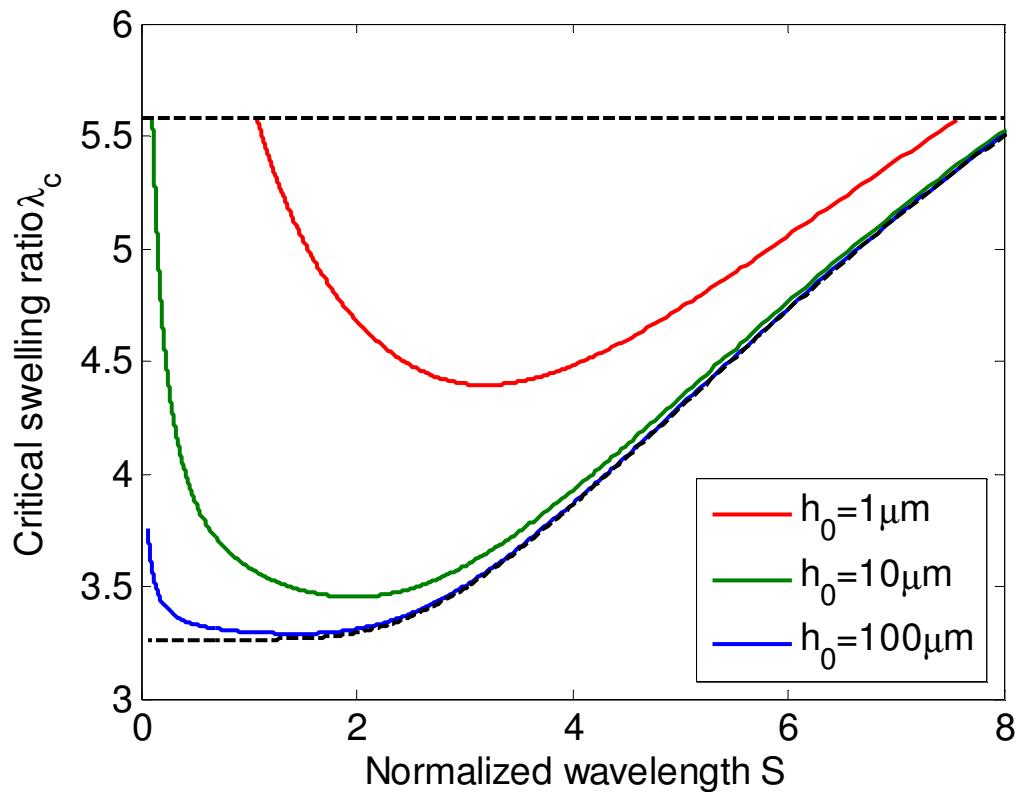


- Trujillo et al.'s experiments for a swelling hydrogel
- Biot's analysis for rubber under equi-biaxial compression

# Effect of surface tension

A length scale:

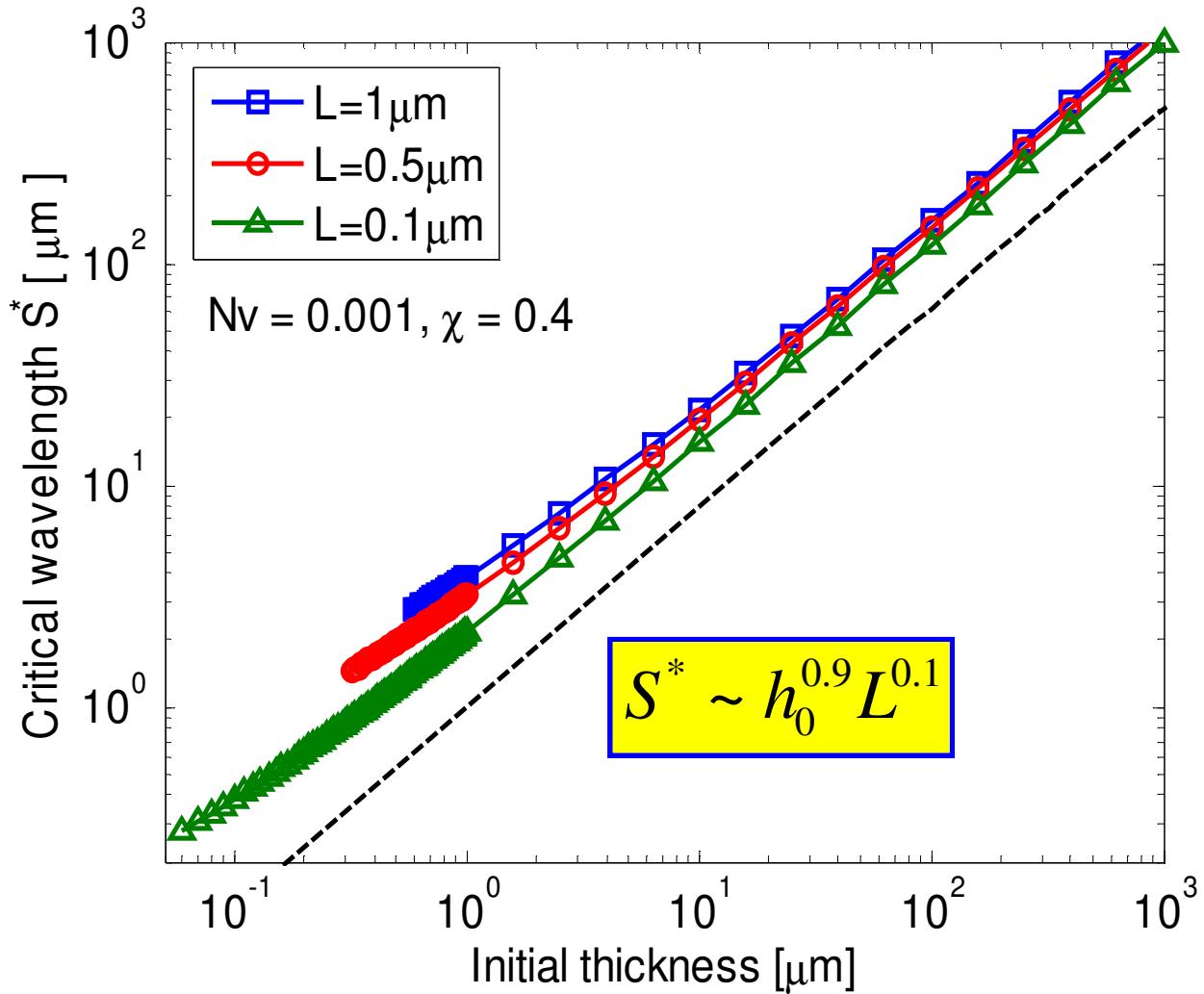
$$L = \frac{\gamma}{Nk_B T} \sim \frac{0.53\text{nm}}{N\nu}$$



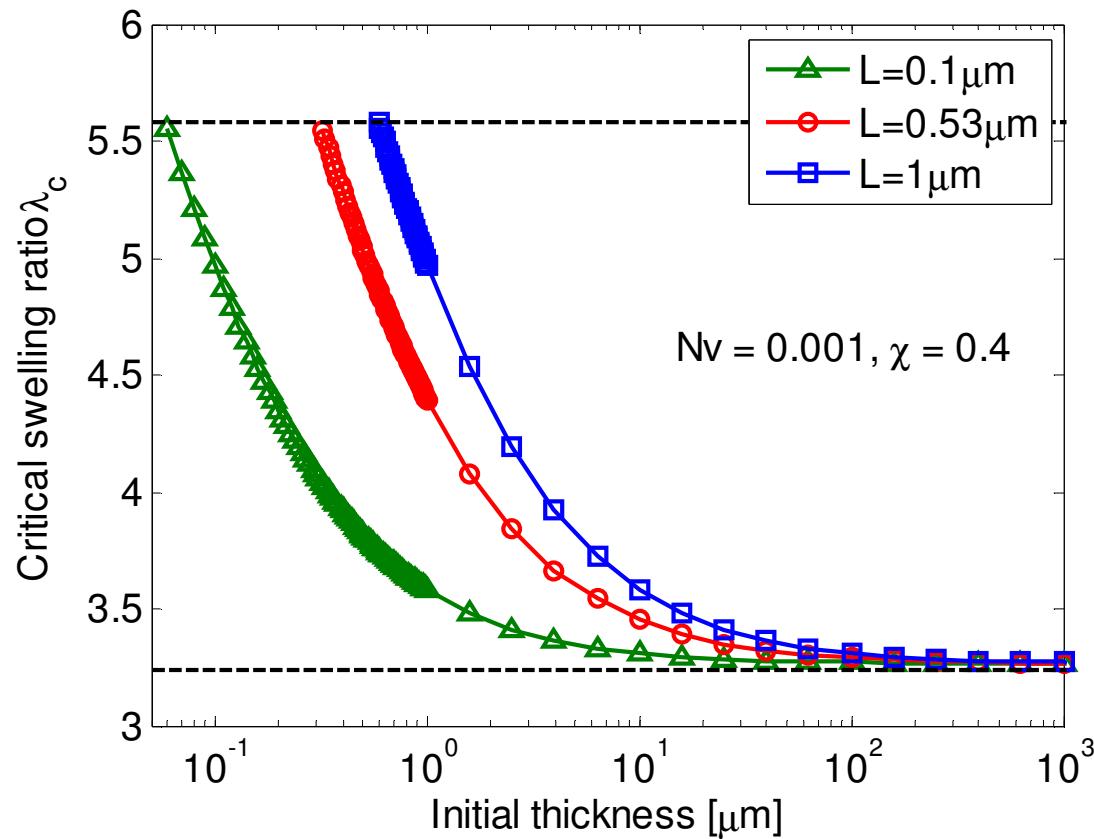
$$N\nu = 0.001, \chi = 0.4$$

- Long wavelength perturbation is stabilized by the substrate.
- Short wavelength perturbation is stabilized by surface tension.
- An intermediate characteristic wavelength emerges.
- The minimum critical swelling ratio depends on the layer thickness.

# Characteristic wavelength



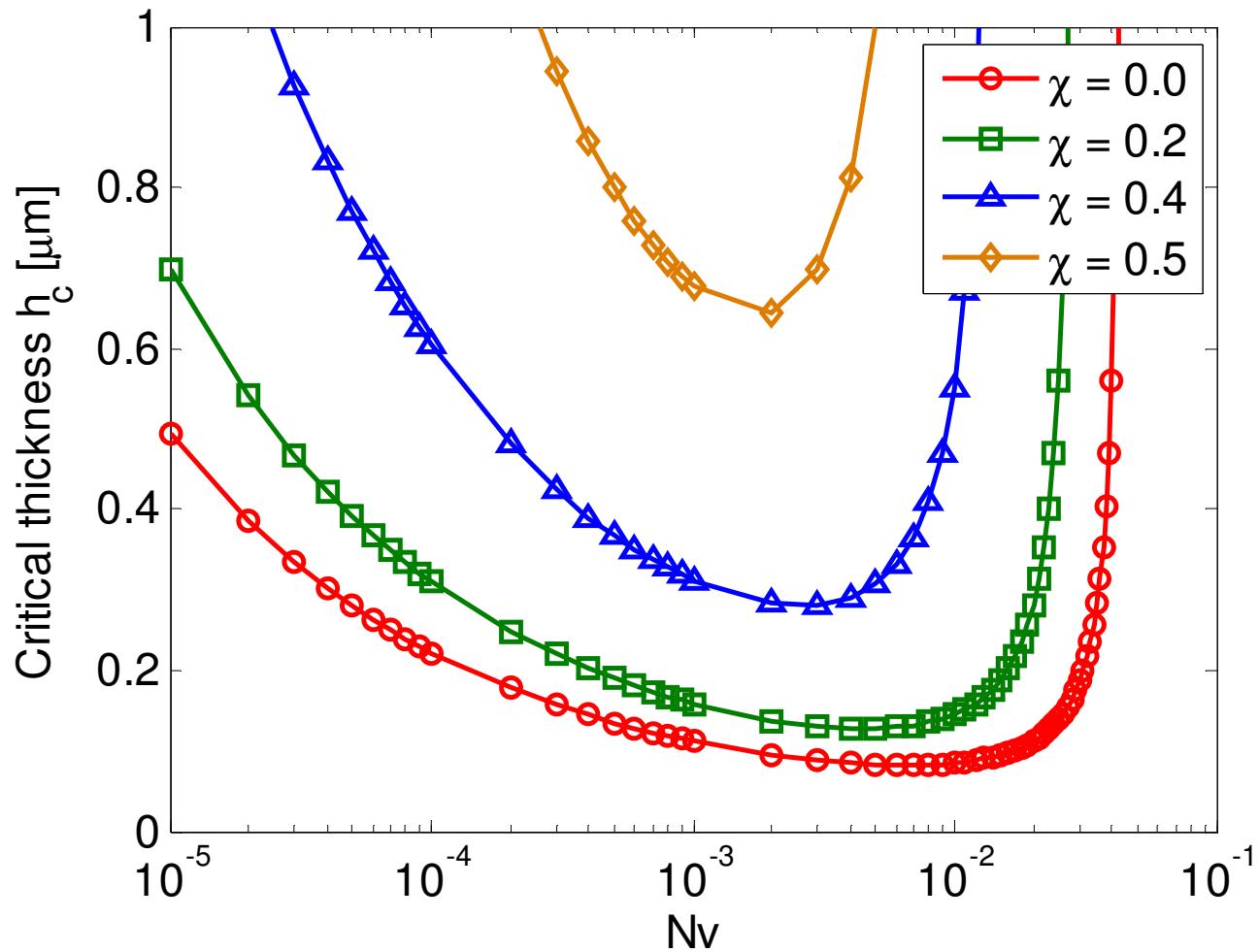
# Thickness-dependent stability



- The hydrogel layer becomes increasingly stable as the initial layer decreases;
- Below a critical thickness ( $h_c$ ), the hydrogel is stable at the equilibrium state.

Kang and Huang, Soft Matter 6, 5736-5742 (2010).

# Critical thickness

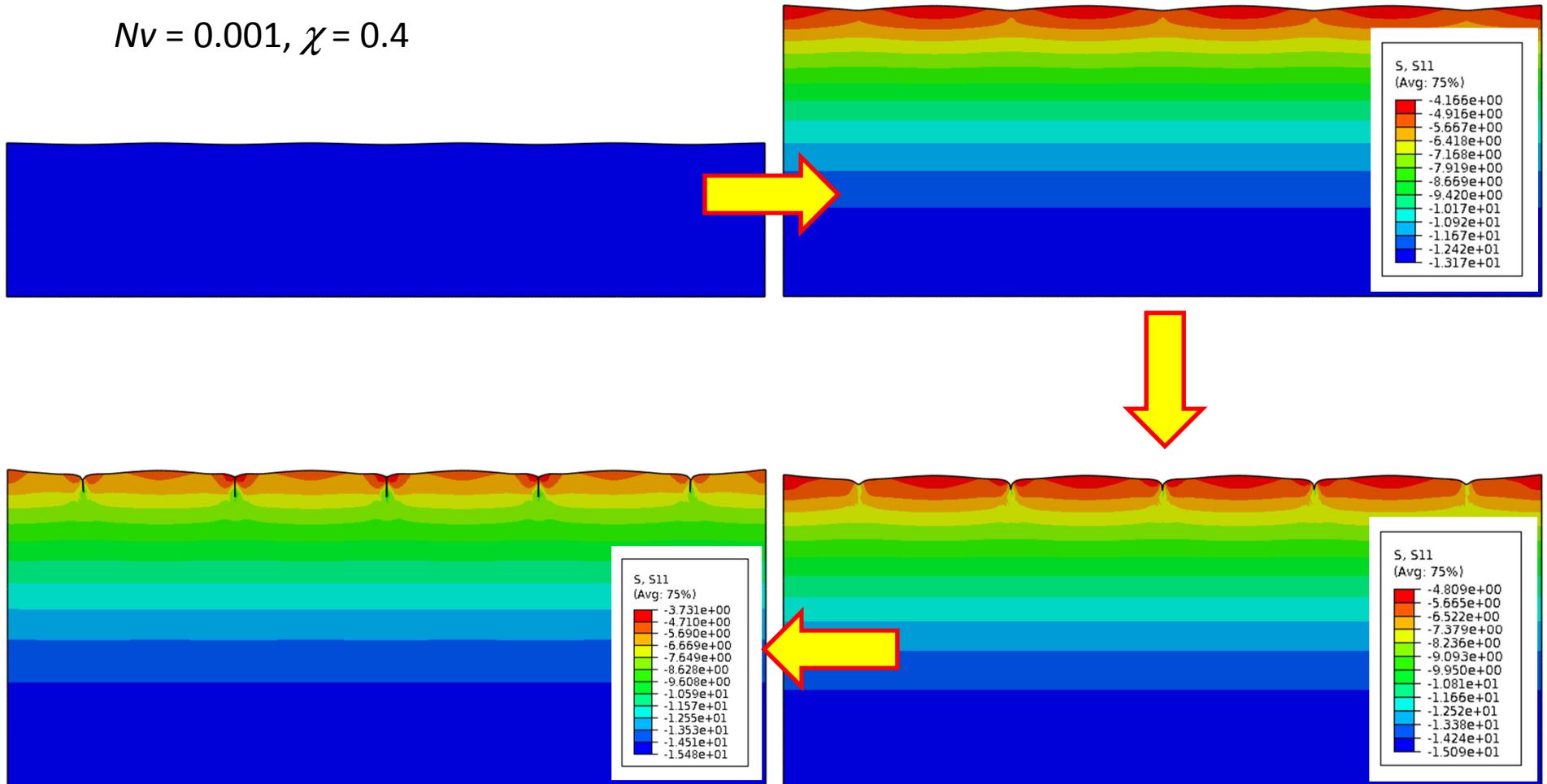


$$L' = \frac{\mathcal{W}}{k_B T} = 0.53\text{nm}$$
$$L = \frac{L'}{Nv}$$

- The critical thickness is linearly proportional to  $L$ , with the proportionality depending on  $Nv$  and  $\chi$ .

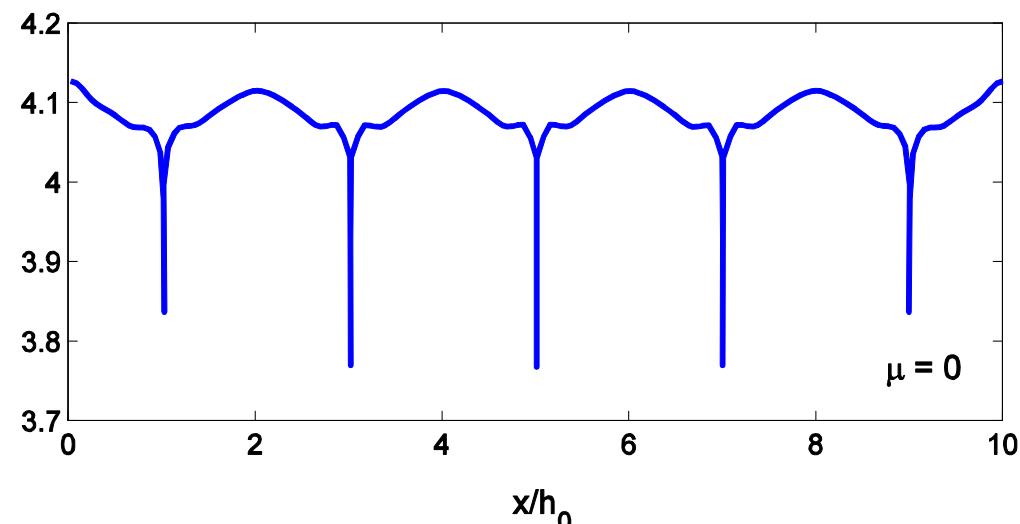
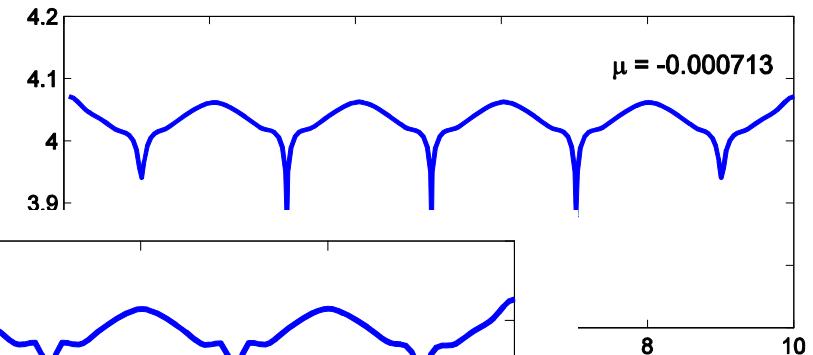
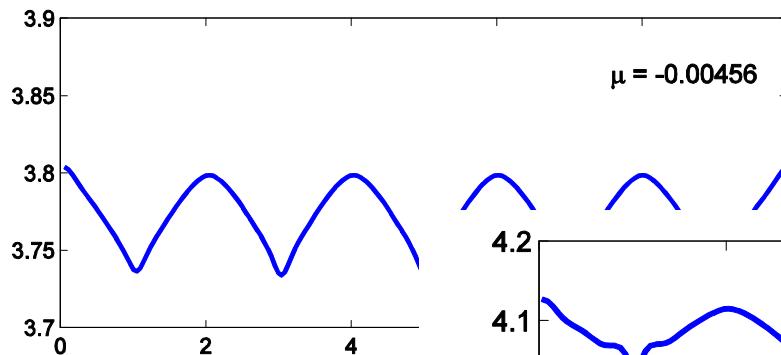
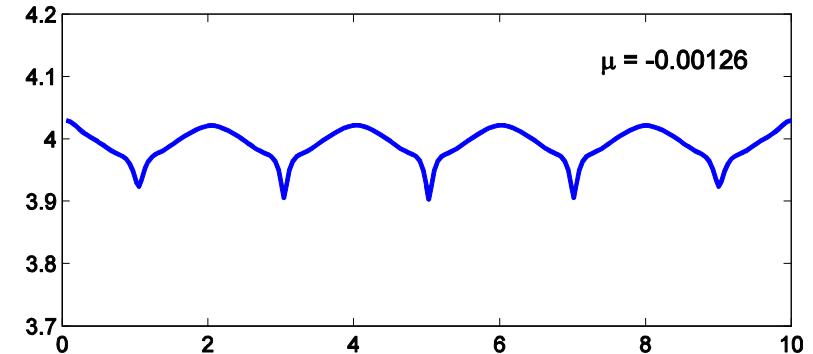
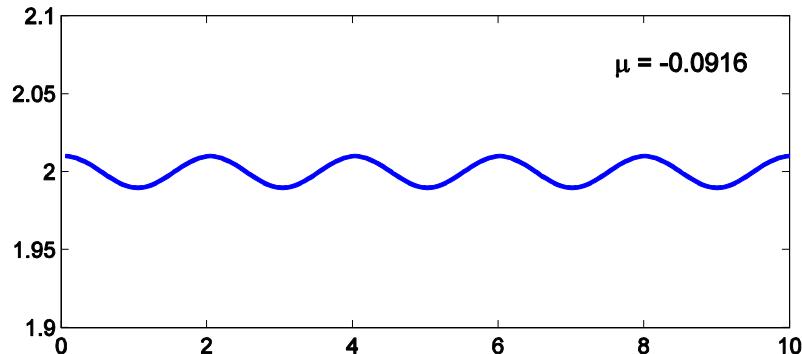
# Finite element simulation

$$Nv = 0.001, \chi = 0.4$$



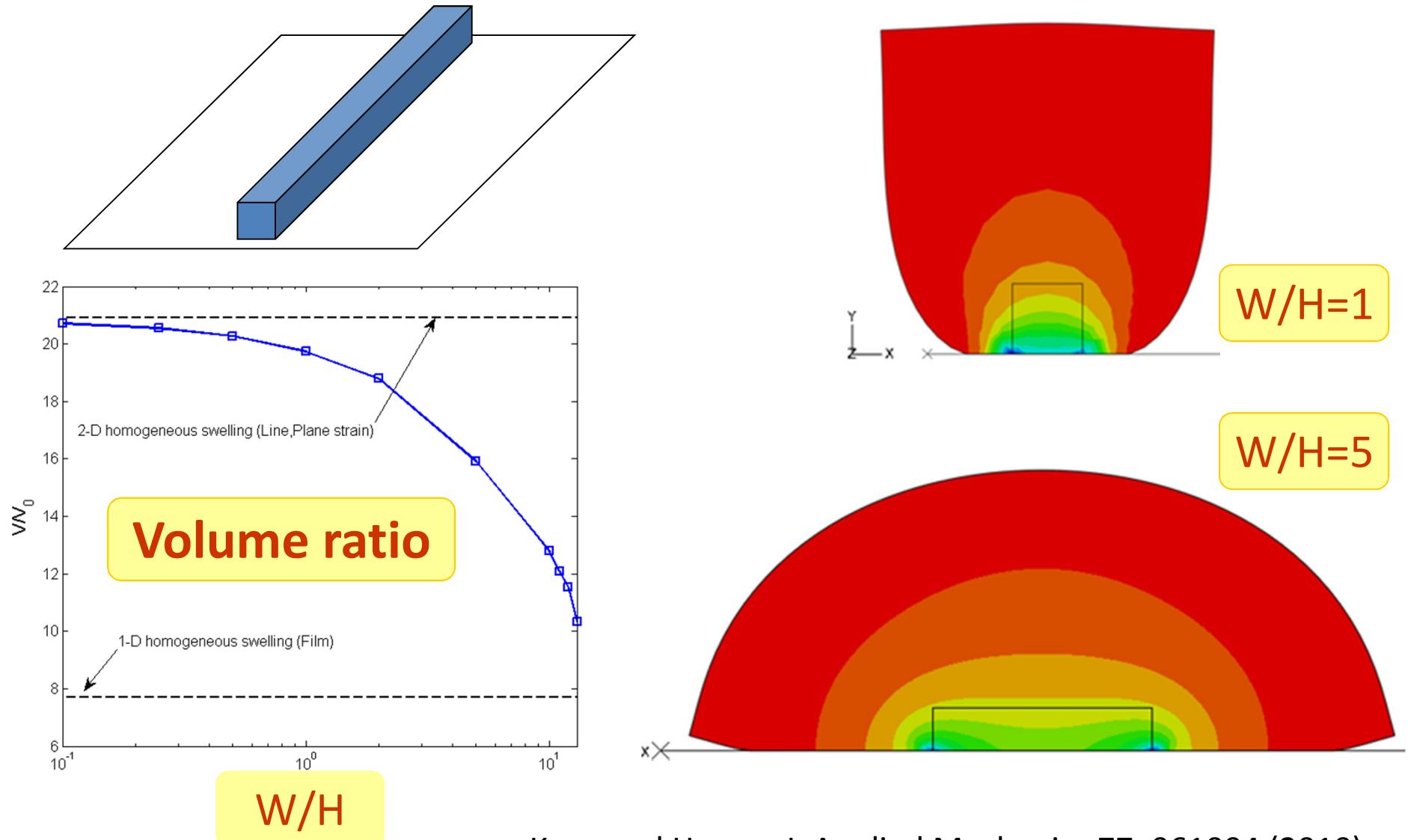
Kang and Huang, J. Mech. Phys. Solids 58, 1582-1598 (2010).

# Surface Evolution



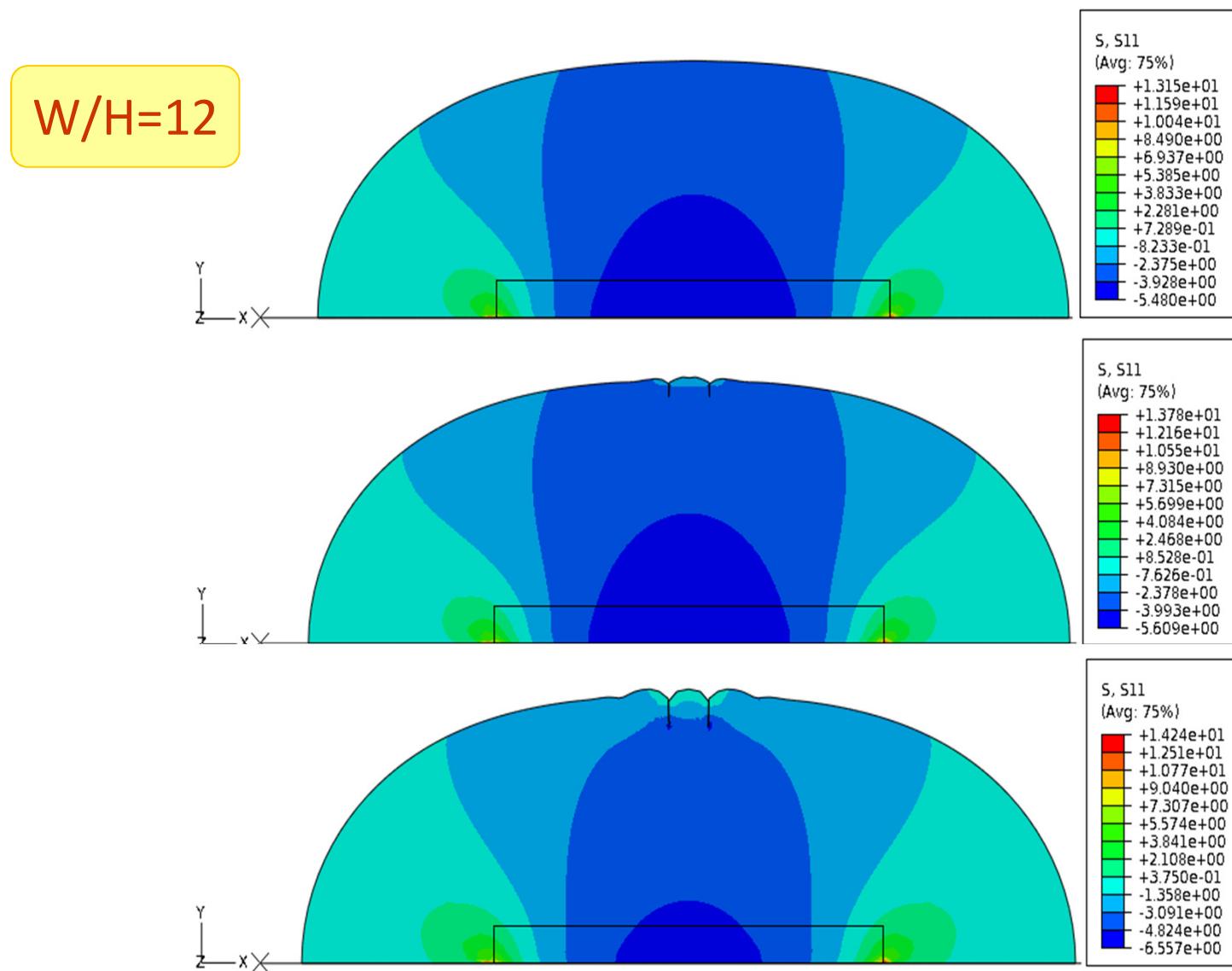
Kang and Huang, J. Mech. Phys. Solids 58, 1582-1598 (2010).

# Inhomogeneous Swelling of Substrate-Supported Hydrogel Lines



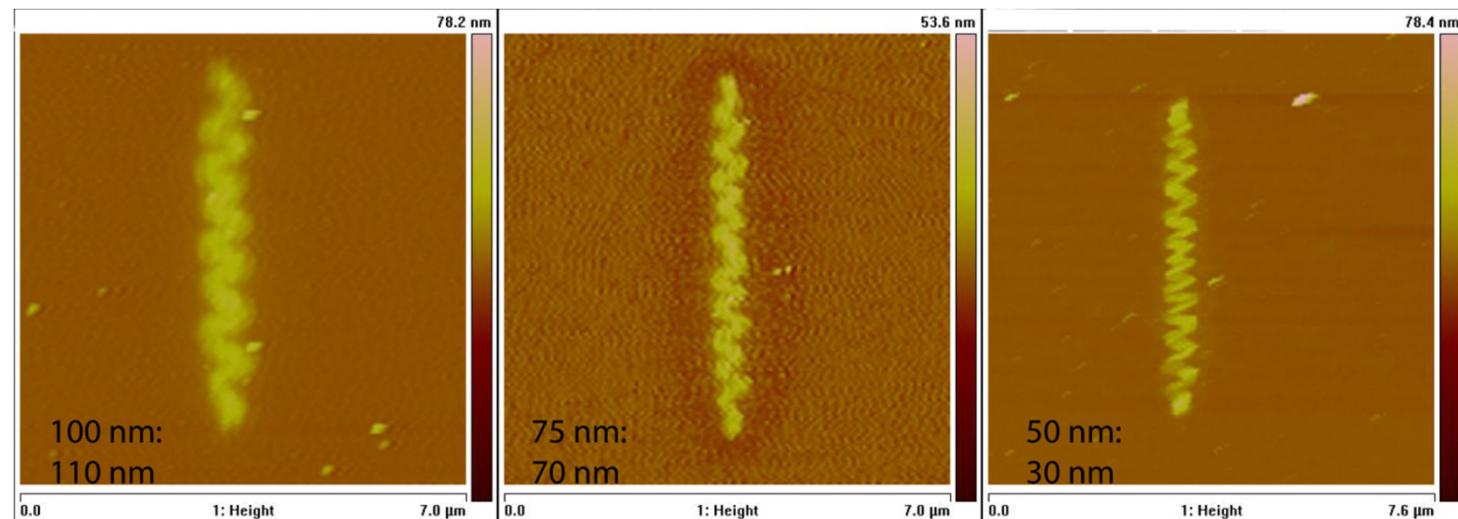
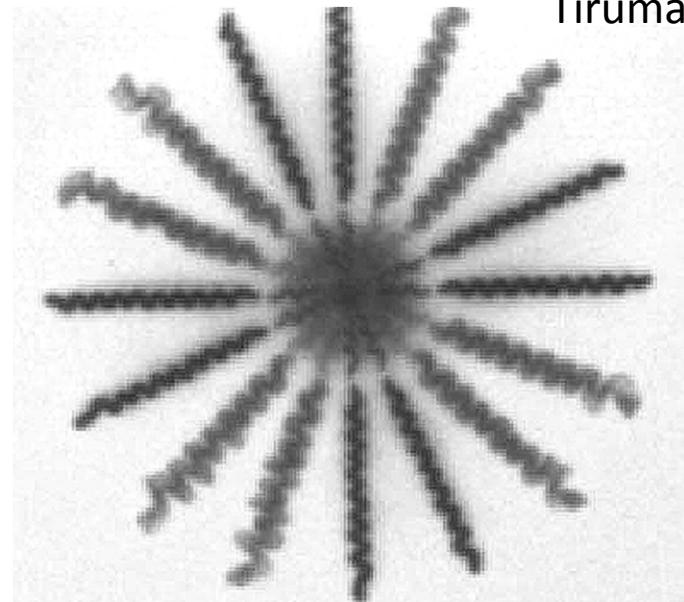
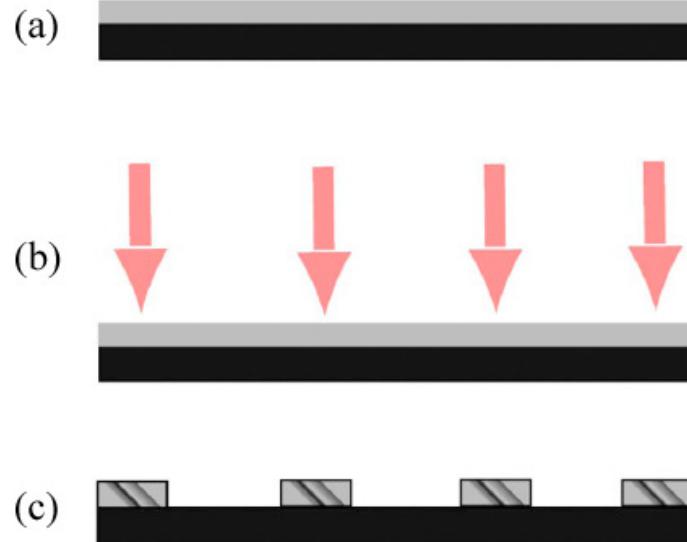
Kang and Huang, J. Applied Mechanics 77, 061004 (2010).

# Spontaneous Formation of Creases

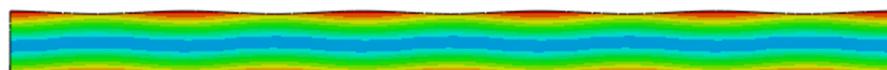


# Swell-induced buckling

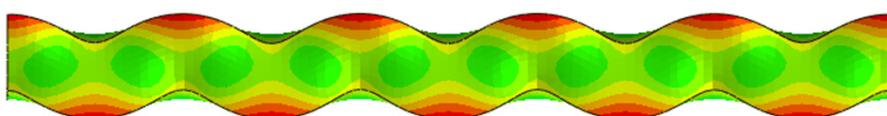
Tirumala et al., 2005



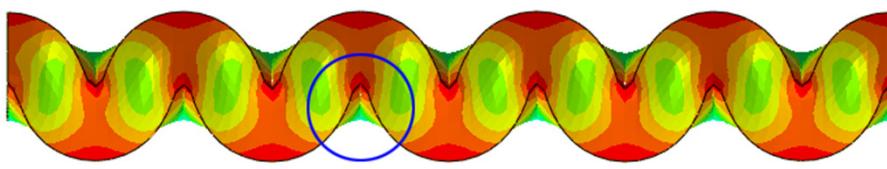
# Effect of material parameters



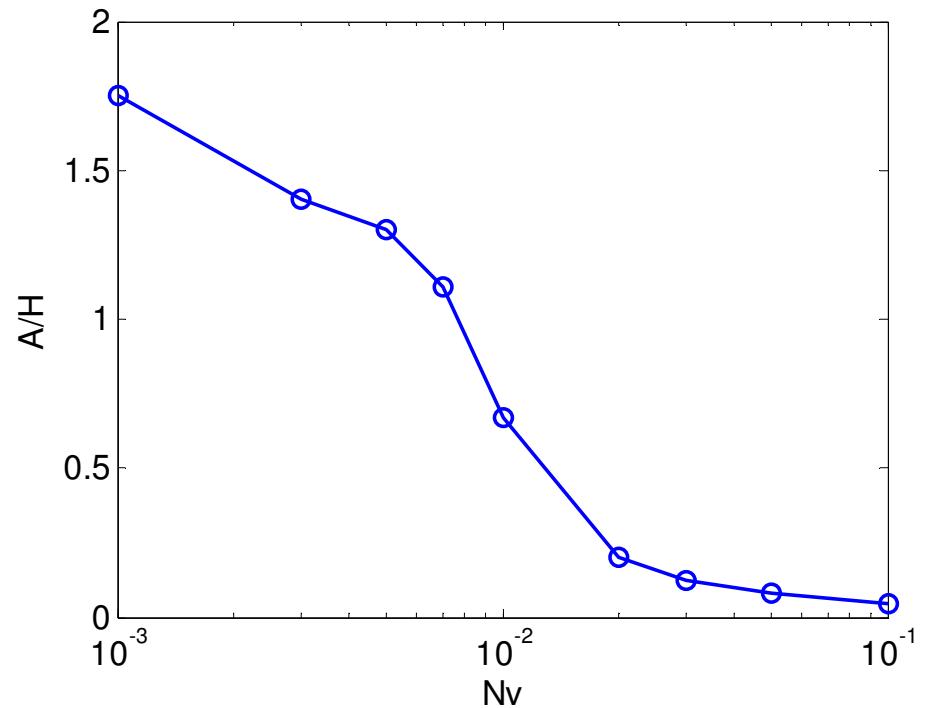
$Nv=0.1, \chi=0.55$



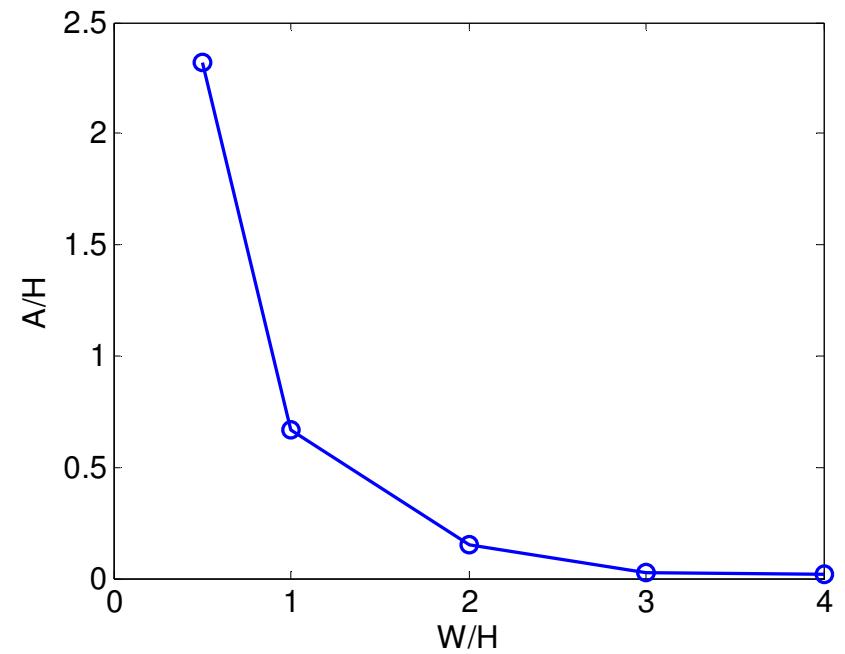
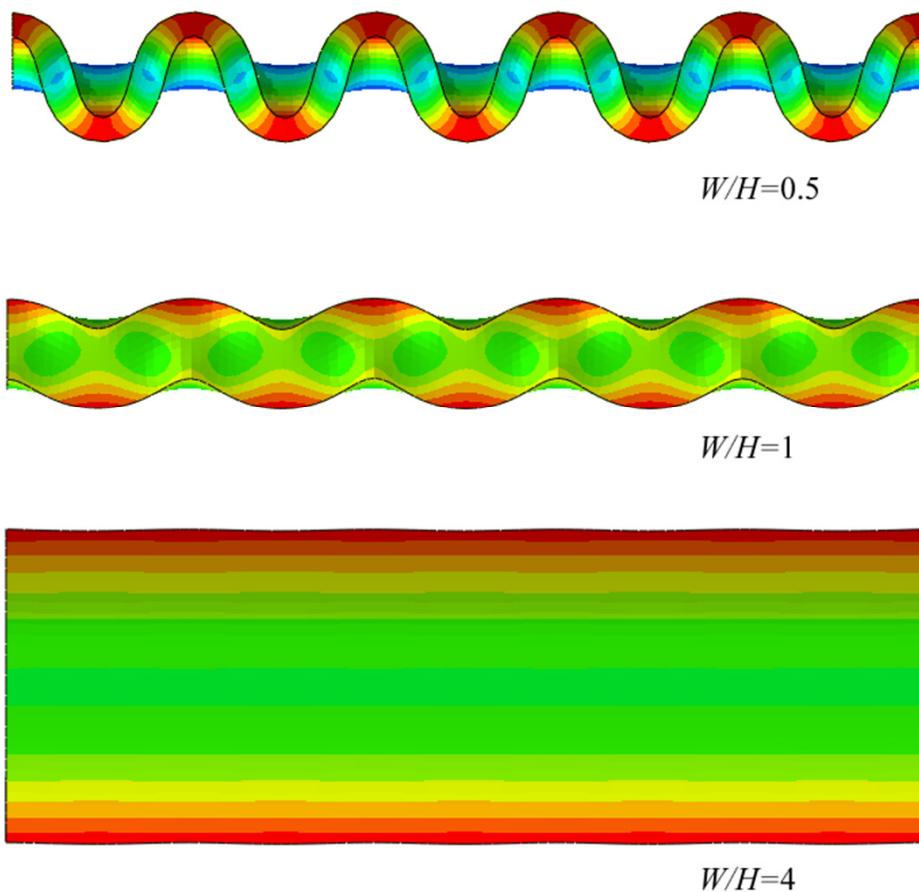
$Nv=0.01, \chi=0.55$



$Nv=0.001, \chi=0.55$



# Effect of geometry (constraint)



# Summary

- **Opportunity:** Within the general theoretical framework, instability of hydrogel-like soft material can be understood and exploited.
- **Challenge:** The highly nonlinear aspects in the material, geometry, and instability mechanics pose serious challenges for theoretical analysis and numerical simulations.
- **Strategy:** Collaborations between experimental and theoretical studies will be most successful.